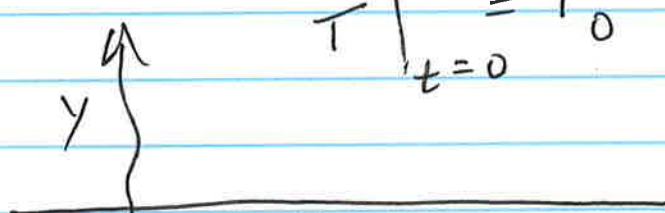


①

Problem of the Day 09

Semi-infinite domain w/ cst. heat flux



$$T|_{t=0} = T_0$$

$$q_y|_{\substack{t>0 \\ y=0}} = q_0 = -k \frac{\partial T}{\partial y} \bigg|_{y=0}$$

So:

$$\rho \hat{C}_p \frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial y^2}$$

$$T^* = \frac{T - T_0}{\Delta T_c} \quad t^* = t/t_c \quad y^* = y/\delta$$

So:

$$\frac{\rho \hat{C}_p \Delta T_c}{t_c} \frac{\partial T^*}{\partial t^*} = \frac{k \Delta T_c}{\delta^2} \frac{\partial^2 T^*}{\partial y^{*2}}$$

Divide:

$$\frac{\delta^2 \rho \hat{C}_p}{t_c k} = \frac{\delta^2}{\alpha t_c}$$

$$\therefore \left[\frac{\delta^2}{\alpha t_c} \right] \frac{\partial T^*}{\partial t^*} = \frac{\partial^2 T^*}{\partial y^{*2}}$$

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$$\text{B.C. : } \left. -\frac{k \Delta T_c}{\delta} \frac{\partial T^*}{\partial y^*} \right|_{y^*=0} = q_0$$

$$\text{or } \left[\frac{k \Delta T_c}{q_0 \delta} \right] \left. \frac{\partial T^*}{\partial y^*} \right|_{y^*=0} = -1$$

$$\text{So } \Delta T_c = \frac{q_0 \delta}{k} \left(= \frac{q_0 (\alpha t_c)^{1/2}}{k} \right)$$

We've rendered eq'n dimensionless and never specified t_c ! \therefore will admit self-similar solution!

Check w/ stretching!

$$\frac{\partial T^*}{\partial t^*} = \frac{\partial^2 T^*}{\partial y^{*2}}; \quad T^* \Big|_{y^* \rightarrow \infty} = 0, \quad T^* \Big|_{t^*=0} = 0$$

$$\left. \frac{\partial T^*}{\partial y^*} \right|_{y^*=0} = -1$$

$$\text{Let } T^* = A \bar{T}, \quad t^* = B \bar{t}, \quad y^* = C \bar{y}$$

$$\frac{A}{B} \frac{\partial \bar{T}}{\partial \bar{t}} = \frac{A}{c^2} \frac{\partial^2 \bar{T}}{\partial \bar{y}^2}$$

Divide out!

$$\frac{\partial \bar{T}}{\partial \bar{t}} = \left[\frac{B}{c^2} \right] \frac{\partial^2 \bar{T}}{\partial \bar{y}^2}$$

In homogeneous BC: $\frac{A}{c} \frac{\partial \bar{T}}{\partial \bar{y}} \bigg|_{\bar{y}=0} = -1$

$$\therefore \frac{A}{c} = 1$$

Canonical Form: complexity in t^* (B)

$$\therefore \frac{c}{B^{1/2}} = 1 \quad \frac{A}{B^{1/2}} = 1$$

$$\therefore \frac{T^*}{t^{*1/2}} = f(\zeta) \quad \zeta = \frac{y^*}{t^{*1/2}}$$

Now for D.E.:

$$T^* = t^{*1/2} f(\zeta)$$

$$\therefore \frac{\partial T^*}{\partial y^*} = t^{*1/2} f' \frac{\partial \zeta}{\partial y^*} = t^{*1/2} f' \frac{1}{t^{*1/2}} = f'!$$

$$\text{B.C. : } \underline{f'(0) = -1}$$

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$$\frac{\partial^2 T^*}{\partial y^{*2}} = \frac{\partial}{\partial y^*} (f') = f'' \frac{1}{t^{*1/2}}$$

Now for time deriv!

$$\begin{aligned} \frac{\partial T^*}{\partial t^*} &= \frac{\partial}{\partial t^*} (t^{*1/2} f) = \frac{1}{2} t^{*-1/2} f + t^{*1/2} \frac{\partial f}{\partial t^*} \\ &= \frac{1}{2} t^{*-1/2} (f - 3f') \end{aligned}$$

So the DE is:

$$f'' = \frac{1}{2} (f - 3f')$$

$$f'(0) = -1, \quad f(\infty) = 0$$

$$\text{and } T = \frac{g_0 (\alpha t)^{1/2}}{k} f\left(\frac{y}{(\alpha t)^{1/2}}\right) + T_0$$

Ok, how to get f ? Easiest to do

numerically, but we can actually get an analytic sol'n with a trick

Take derivative of ODE!

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$$\frac{d}{dz} \left\{ f'' = \frac{1}{2} (f - 3f') \right\}$$

$$\therefore f''' = \frac{1}{2} (\cancel{f} - \cancel{f'} - 3f'')$$

$$\text{so } f''' = -\frac{1}{2} 3f''$$

Divide by f'' :

$$\frac{f'''}{f''} \equiv \frac{d \ln f''}{dz} = -\frac{1}{2} 3$$

$$\text{so } \ln f'' = -\frac{1}{4} z^2 + \text{cst}$$

$$f'' = \frac{1}{2} f(0) e^{-\frac{1}{4} z^2}$$

↑
from original DE eval. at
 $z = 0$

(we don't know $f(0)$)

We could integrate twice and get
in terms of $\text{ierfc}(x)$, the
integral complementary error function...

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Instead, just do it numerically!

$$\vec{f} = \begin{bmatrix} f_1 \\ f_2 \end{bmatrix} = \begin{bmatrix} f \\ f' \end{bmatrix}$$

$$\frac{d\vec{f}}{dz} = \begin{bmatrix} f_2 \\ +\frac{1}{2}(f_1 - 3f_2) \end{bmatrix}$$

$$\vec{f}(0) = \begin{bmatrix} x \\ -1 \end{bmatrix} \leftarrow \text{unknown}$$

Iterate until $f_1(\infty) = 0$!

~~After~~

After a second or two, we get $f_1(0) = \underline{1.184}$
(a nice $O(1)$ number!)

We are actually interested in
plotting lines of constant temperature
~~for different~~ as a function of time!

This will yield the melt zone!

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Let T_m = melting temperature

$$\therefore T_m^* = \frac{T_m - T_0}{\Delta T_c}$$

We seek to determine y^* (or z)
for which $T^* = T_m^*$ at a particular
time t^* . This would be some z_m
that is a function of t^* :

$$T_m^* = t^{*1/2} f(z_m)$$

$$y^* = z_m t^{*1/2}$$

Note that $f(z)$ has a max of 1.128
so we only exceed T_m^* (and start
to melt) if $t^* > \left(\frac{T_m^*}{f(0)} \right)^2$

$$\text{or } t > \cancel{t_c} \left(\frac{T_m - T_0}{f(0)} \right)^2 \left(\frac{15}{9_0} \right)^2 \left(\frac{1}{\cancel{\Delta T_c}} \right)$$

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$$\text{or } t > \left(\frac{T_m - T_0}{f(0)} \right)^2 \frac{R^2}{q_0^2 \alpha}$$

After this time the melt zone would propagate through the slab!

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Heated Semi infinite slab: Constant Wall Heat Flux

The miss2 program is:

function out = miss2(x) % This function takes in a guess for the derivative of the temperature at % y = 0 for an impulsively heated semi-infinite domain, but with heat flux % at the wall this time.

```
fdot = @(eta,f) [f(2); 0.5*(f(1)-eta*f(2))]; %The differential equation
```

```
f0 = [x,-1]; %The initial value
```

```
[etaout fout] = ode45(fdot,[0 10],f0);
```

```
out = fout(end,1);
```

```
x = 1; % Our initial guess for the temperature at the wall
```

```
x = fzero('miss2',x) % Our solution!
```

```
x =
```

```
1.1284
```

Plotting things up

We just cut and paste from the miss.m routine to get the profile:

```
fdot = @(eta,f) [f(2); 0.5*(f(1)-eta*f(2))]; %The differential equation
```

```
f0 = [x,-1]; %The initial value
```

```
[etaout fout] = ode45(fdot,[0 10],f0);
```

```
out = fout(end,1);
```

```
figure(1)
```

```
plot(etaout,fout(:,1))
```

```
xlabel('eta')
```

```
ylabel('dimensionless temperature')
```

```
title('Temperature Distribution for Constant Heat Flux')
```

```
axis([0 5 0 1.5])
```

```
grid on
```

